



An Introduction to Ion-Optics

Series of Five Lectures
JINA, University of Notre Dame
Sept. 30 – Dec. 9, 2005

Georg P. Berg

The Lecture Series

1st Lecture: 9/30/05, 2:00 pm: Definitions, Formalism, Examples

2nd Lecture: 10/7/05, 2:00 pm: Ion-optical elements, properties & design

3rd Lecture: 10/14/05, 2:00 pm: Real World Ion-optical Systems

4th Lecture: 12/2/05, 2:00 pm: Separator Systems, Part 1

5th Lecture: 12/9/05, 2:00 pm: Separator Systems, Part 2

5th Lecture

5th Lecture: 12/2/05, 2:00 pm
Separator Systems

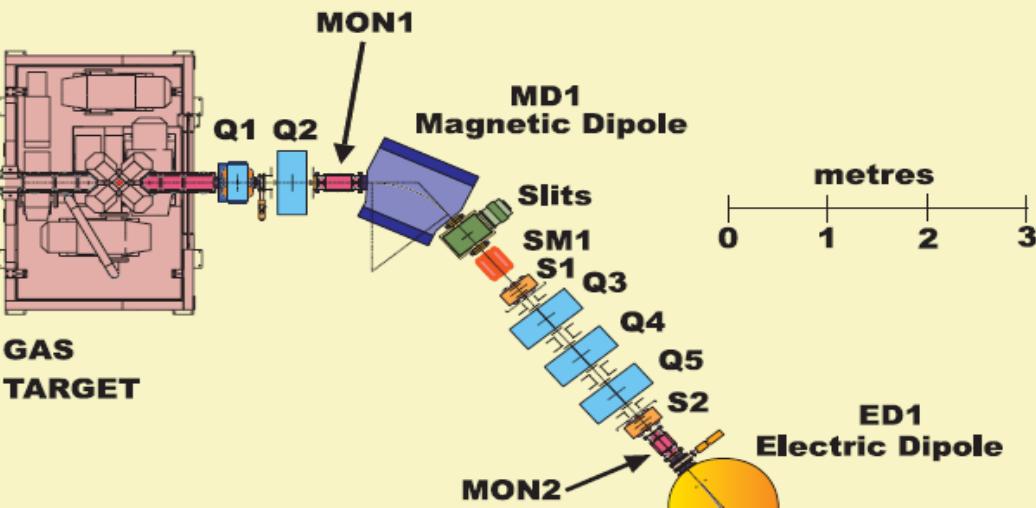
- Electric Dipoles in Recoil Separator Dragon & EMMA
- Wien Filter in Recoil Separators
- Recoil separators ERNA and ARES for astrophysics
- A “no-field” separation method: the Wedge
- In-flight isotope separators TRI μ P and A1900
- Gas-filled separators
- Astrophysics recoil separator St. George

DRAGON

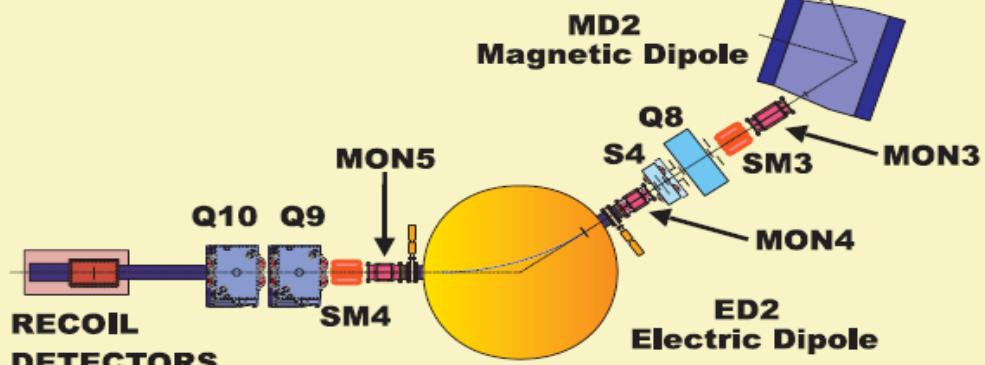
Recoil Separator with Electric Dipoles

Study of astrophysics reactions
using radioactive beams:

e.g. $^{21}\text{Na}(\text{p},\gamma)^{22}\text{Mg}$ in inverse
kinematics using a radioactive
 ^{21}Na beam of 4.62 MeV to
study NeNa cycle

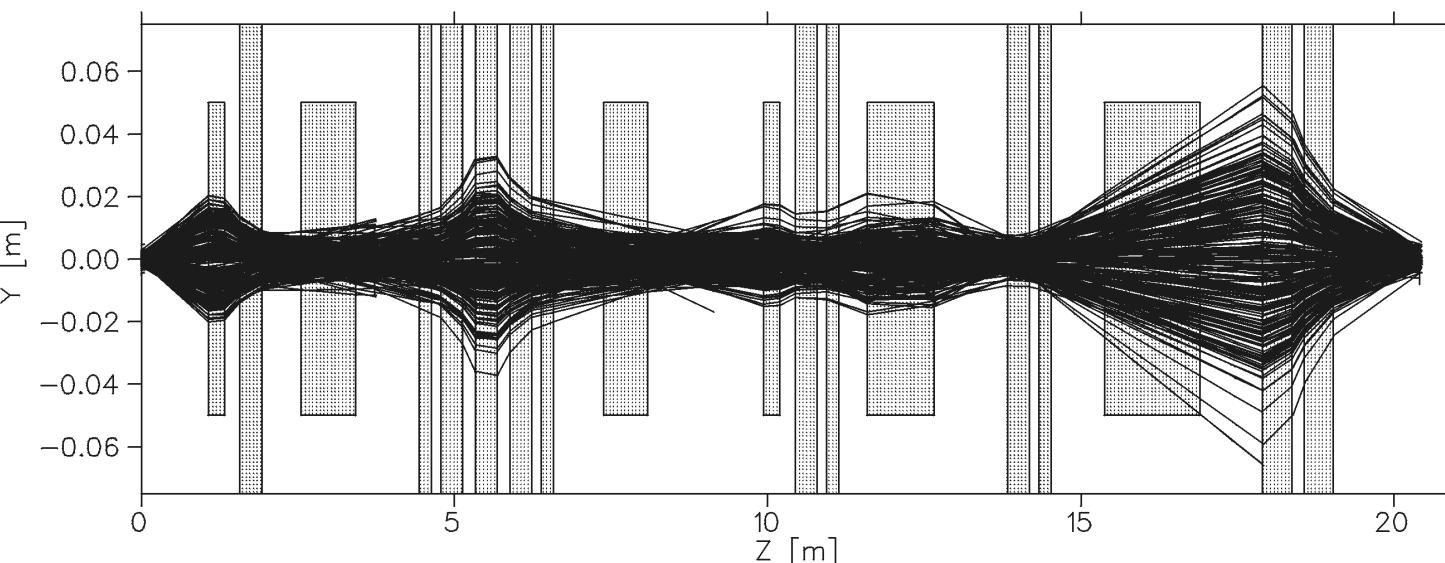
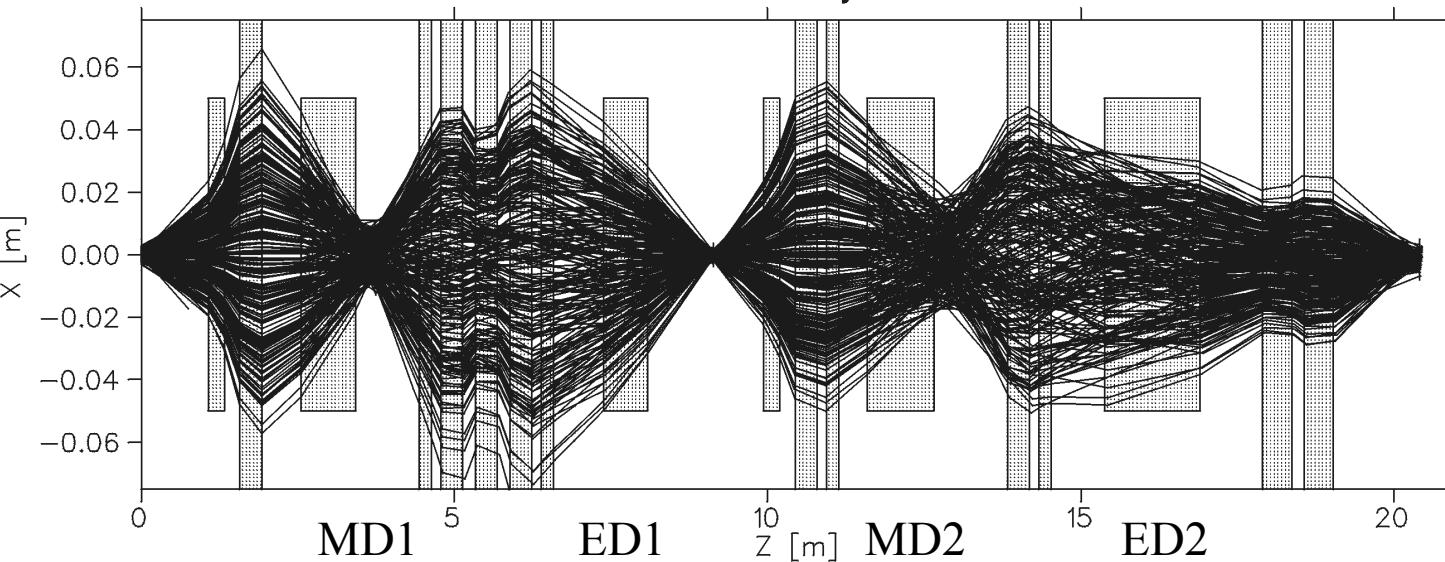


DRAGON
(Detector of Recoils And
Gammas Of Nuclear reactions)



Ref. Dragon Recoil
Separator Optics,
The Recoil Group,
1/18/1999, TRIUMF

Horizontal and Vertical projections of ^{19}Ne trajectories



Ref. J. M. D'Auria et al.
TRIUMF

EMMA

Recoil Separator for ISAC-II at TRIUMF

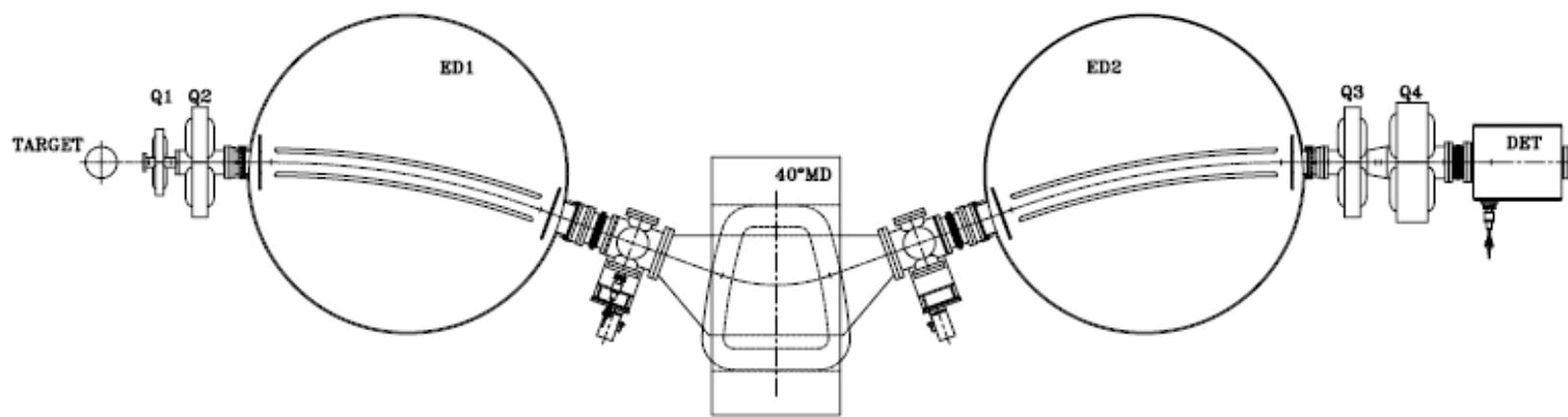
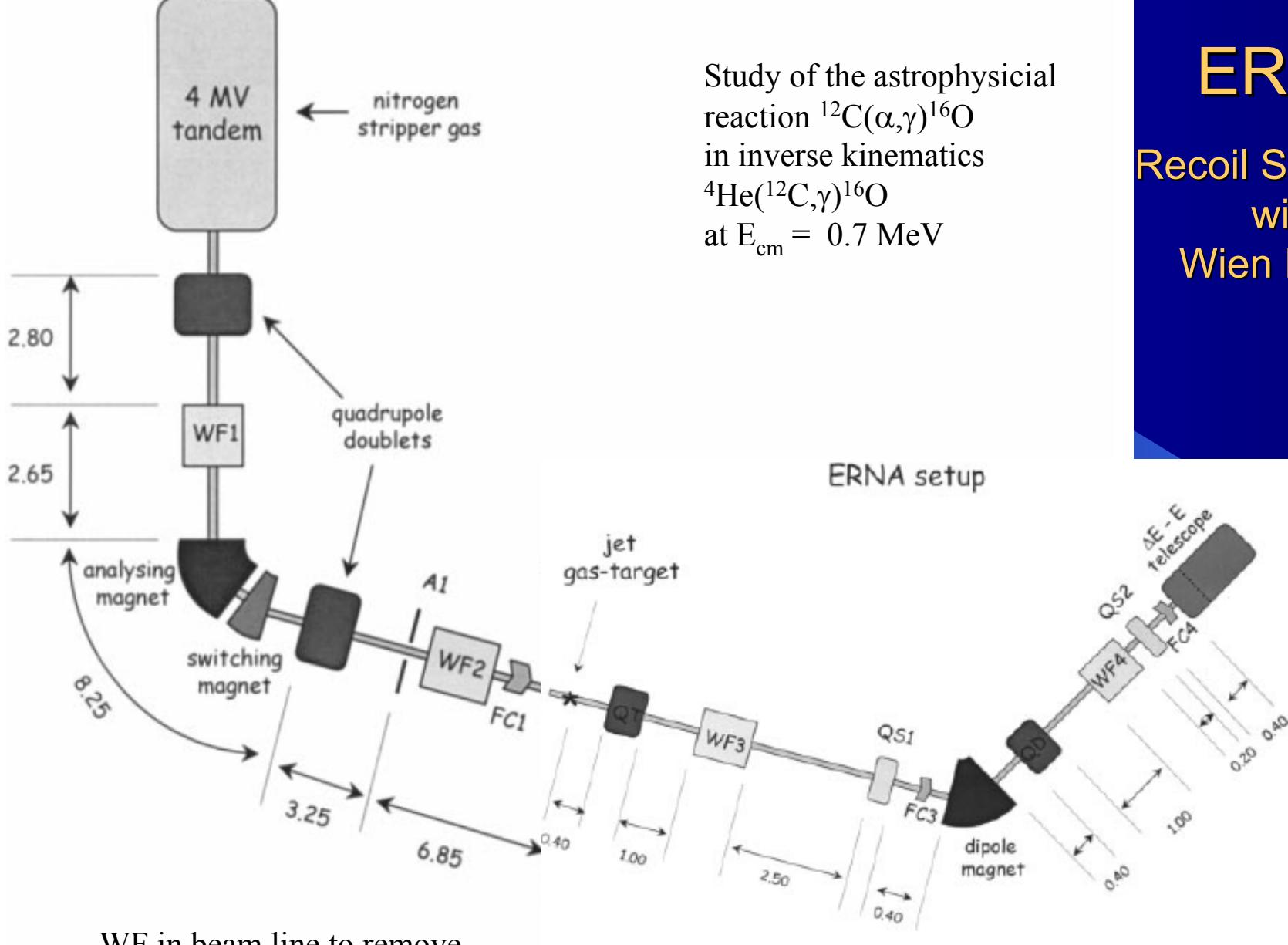


Fig. 1. Schematic view of EMMA, showing the target, quadrupole and dipole magnets, and electric dipoles. The detector box is also indicated.

B. Davids, TRIUMF &
C. Davids, ANL

ERNA

Recoil Separator with Wien Filters



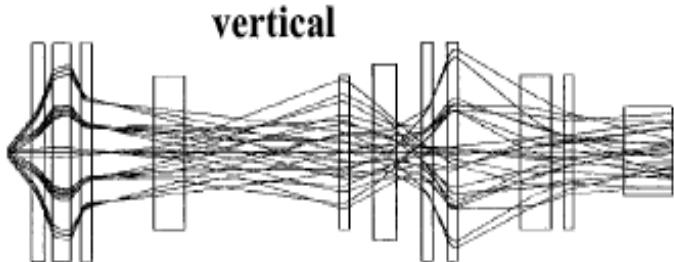
WF in beam line to remove
 ^{16}O contaminant in ^{12}C beam

beam purification

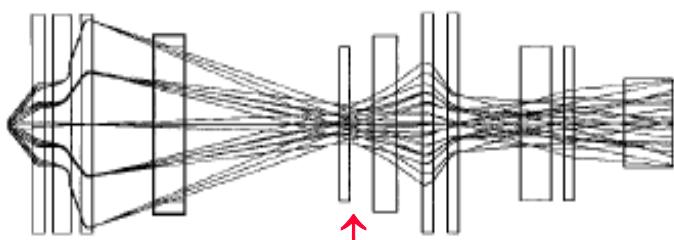
ERNA Recoil Separator with
2 Wien Filters WF3, WF4

Recoil Separator with Wien Filters

a) $^{16}\text{O}^{3+}$ trajectories at $E = 0.70 \text{ MeV}$

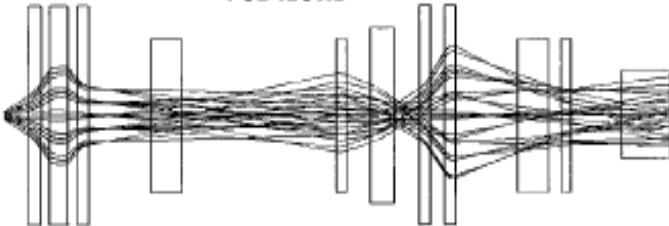


horizontal

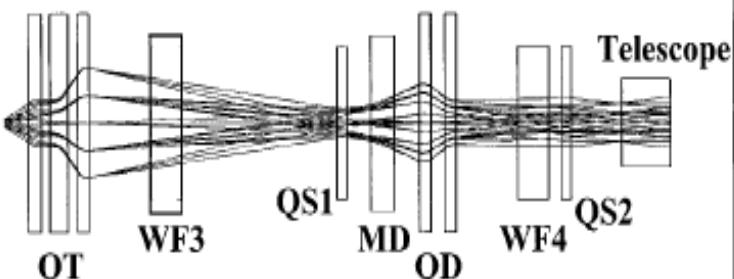


b) $^{16}\text{O}^{6+}$ trajectories at $E = 5.00 \text{ MeV}$

vertical



horizontal



Ion-optics of
 $^{16}\text{O}^{3+}$ and 6^+ ions

3rd order calculations using
COSY Infinity

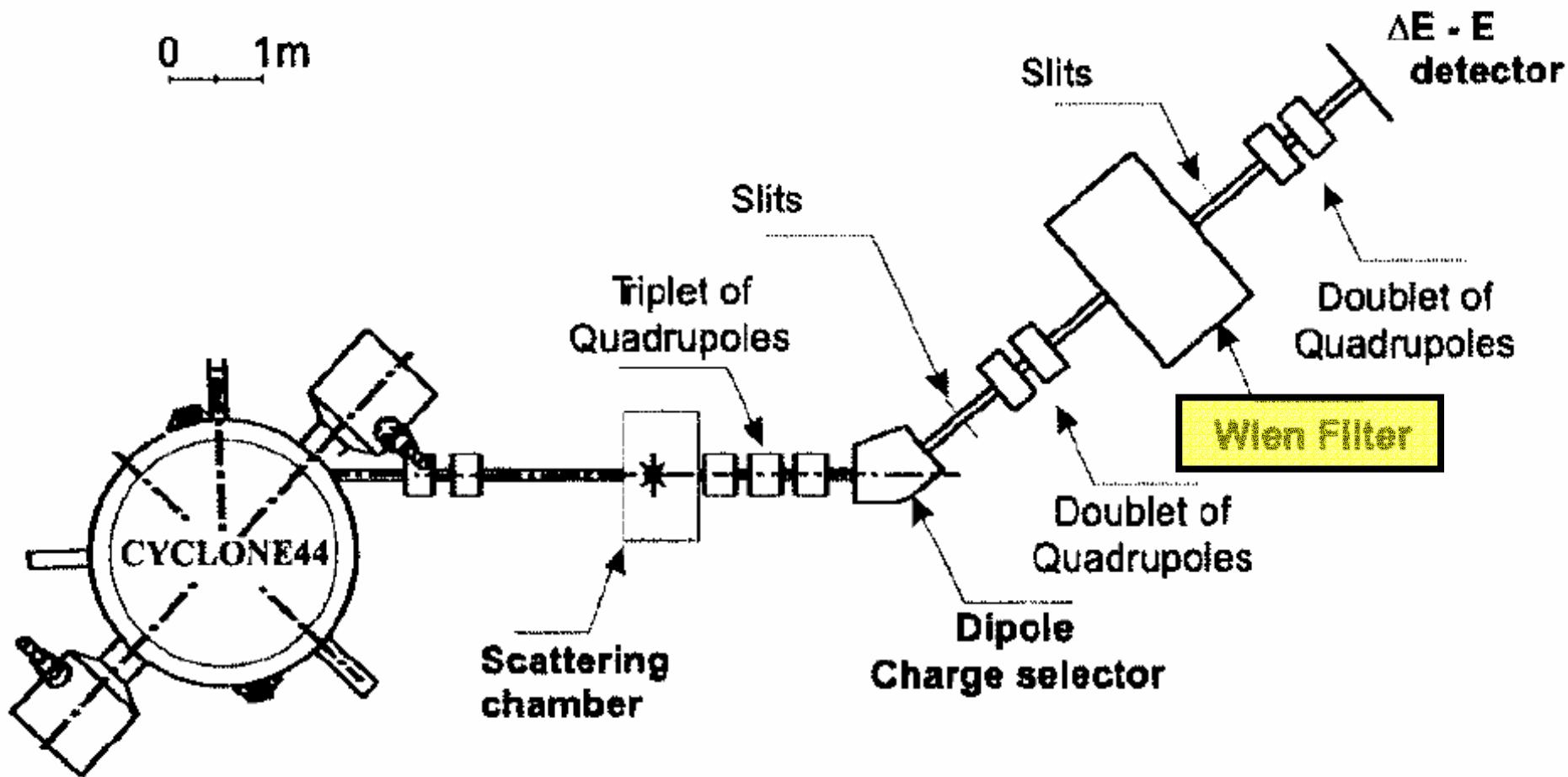
^{12}C beam mainly stopped in
Faraday cup between QS1 and MD

Fig. 2. Samples of ^{16}O trajectories are shown for (a) $E = 0.70 \text{ MeV}$ ($q_0 = 3^+$, $\theta_{\max} = 1.9^\circ$, $\Delta E = 0.13 \text{ MeV}$) and (b) $E = 5.0 \text{ MeV}$ ($q_0 = 6^+$, $\theta_{\max} = 1.0^\circ$, $\Delta E = 0.44 \text{ MeV}$). The trajectories start at the jet gas-target (${}^4\text{He}$ target density = $1 \times 10^{18} \text{ atoms/cm}^2$) and are followed through the filtering and focusing elements of ERNA (indicated by square boxes) up to the telescope (WF = Wien filter, QS = quadrupole singlet, QD = quadrupole doublet, QT = quadrupole triplet, MD = magnetic dipole)

Example: Hot CNO breakout reaction $^{19}\text{Ne}(\text{p},\gamma)^{20}\text{Na}$ in inverse kinematics using a radioactive ^{19}Ne beam of 10.1 MeV

Recoil Separator
with a
Wien Filter

Ref. M. Couder, PhD Thesis July 2004, Louvain-La-Neuve



Achromatic magnet separator

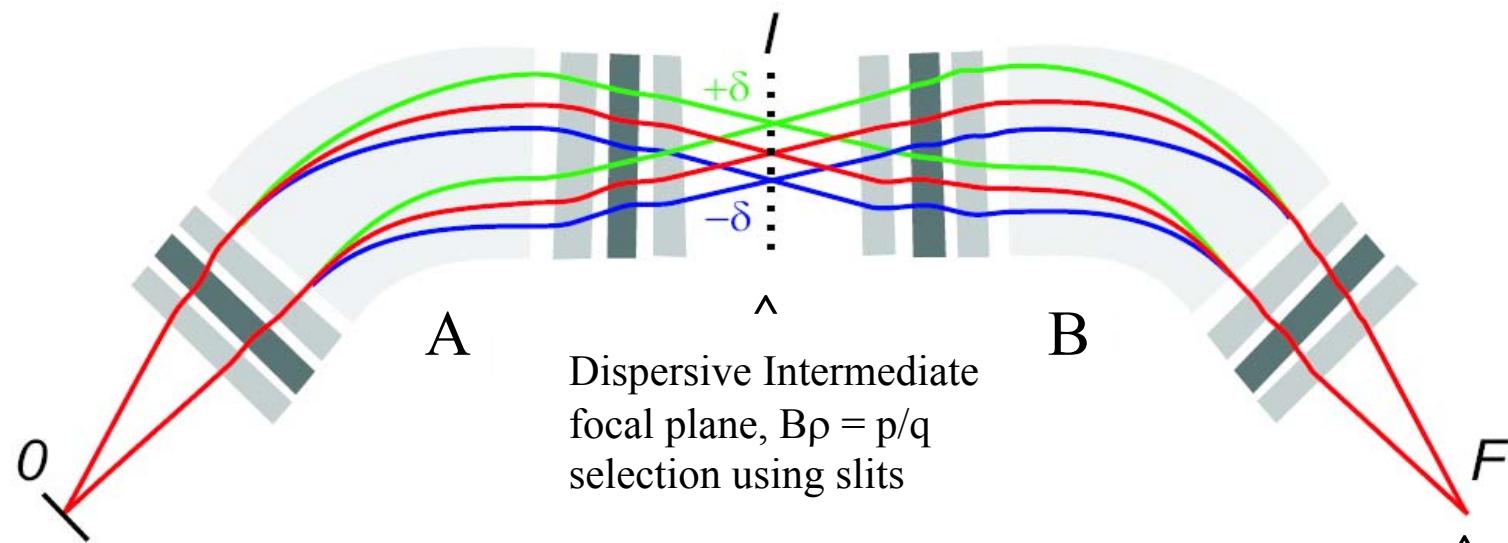


Figure from Experimental Techniques at NSCL, MSU, Th. Baumann, 8/2/2002

Achromatic Final focal plane, small beam spot
e.g. for detector system

Exercise 4:

Assume foci at I & F , i.e. $A_{12} = B_{12} = 0$.

Derive the first order achromatic condition of the system $O \rightarrow F$ and compare with the dispersion matching condition.

Solution of Exercise 4

First order
TRANSPORT
Matrix $R_{\mu\nu}$

	Magnification M_x	Focusing fact	Lateral Dispersion	
$x(t)$	R_{11}	R_{12}	0	0
$\theta(t)$	R_{21}	R_{22}	0	R_{26}
$y(t)$	0	0	R_{33}	x_0
$\varphi(t)$	0	0	R_{34}	θ_0
$l(t)$	R_{43}	R_{44}	0	y_0
$\delta(t)$	R_{51}	R_{52}	0	φ_0
	$\vec{x}_2 = \text{TRANSPORT} \cdot R - \text{Matrix} \cdot \vec{x}_1$			

Angular Disp (2)

$$x_I = A_{11} x_0 + A_{12} \theta_0 + A_{16} \delta_0 \quad | A_{12} = 0$$

$$= A_{11} x_0 + A_{16} \delta_0 \quad \text{(33)}$$

$$x_F = B_{11} x_I + B_{12} \theta_I + B_{16} \delta_0 \quad | B_{12} = 0$$

$$= B_{11} x_I + B_{16} \delta_0 \quad | \text{ substitute } x_I \text{ using (33)}$$

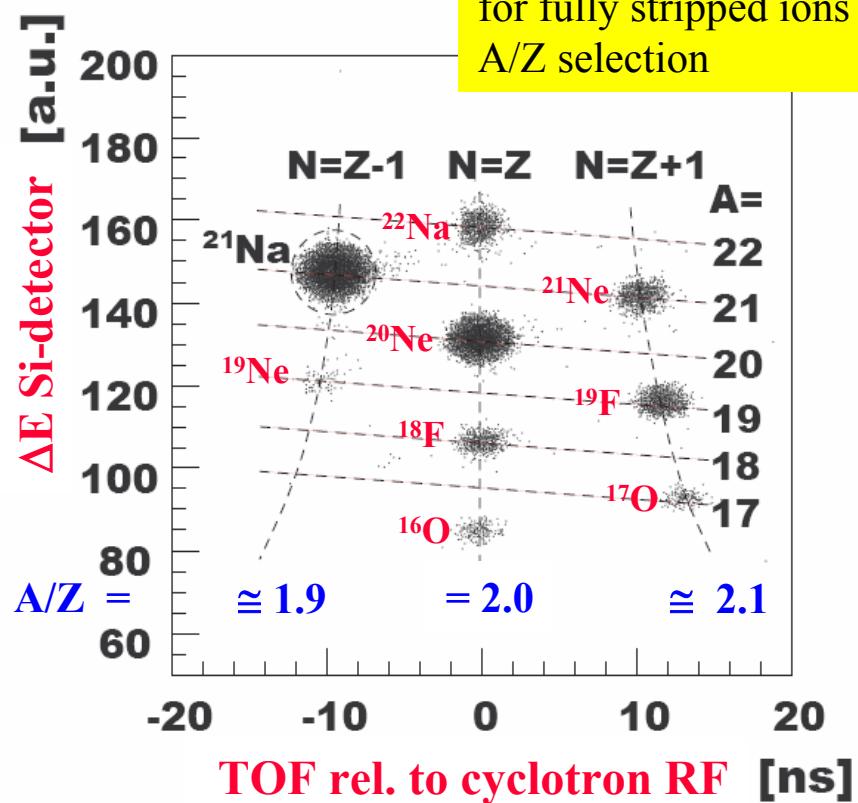
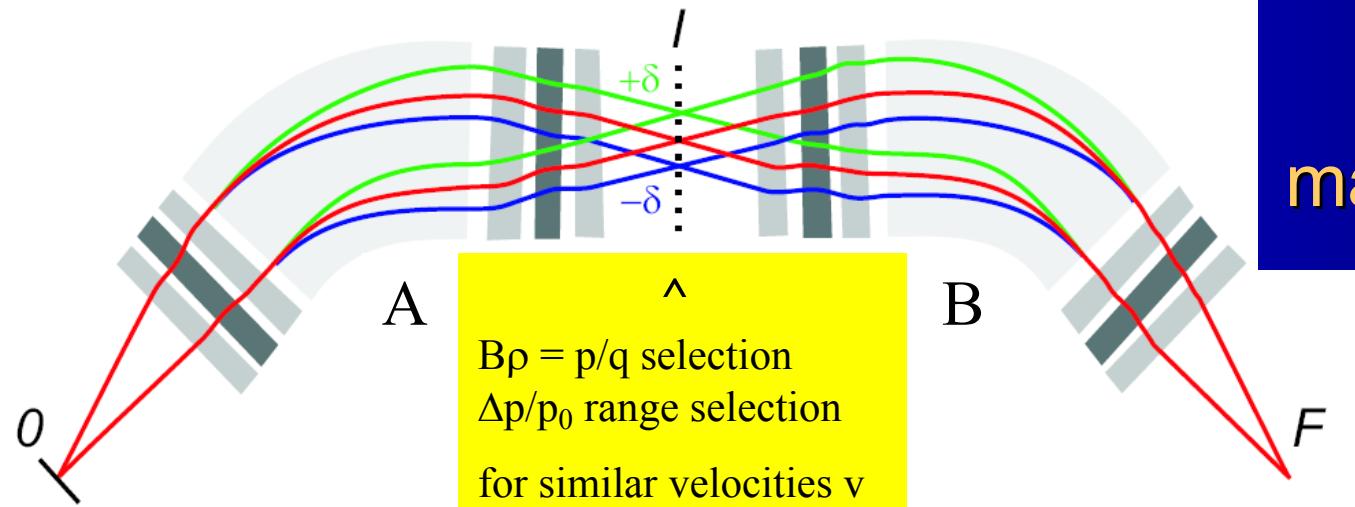
$$= B_{11} (A_{11} x_0 + A_{16} \delta_0) + B_{16} \delta_0$$

$$= B_{11} A_{11} x_0 + (B_{11} A_{16} + B_{16}) \delta_0$$

Condition for achromaticity: $A_{16} = - B_{16} / B_{11}$

Note: This is the Dispersion Matching condition for $C = T = 1$

Achromatic magnet separator



0.1 mm **ΔE Si-detector**
 20 mm diameter

Example: Production of ^{21}Na via $\text{H}(^{21}\text{Ne}, n)^{21}\text{Na}$ with $^{21}\text{Ne}^{7+}$ beam at 43 MeV/nucleon using the TRI μ P Separator, KVI Groningen
 Ions after target fully stripped e.g. $^{21}\text{Ne}^{10+}$!

^{21}Ne beam with $\approx 10^{10}$ ions/s with
 $B\rho(^{21}\text{Ne})/B\rho(^{21}\text{Na}) \approx 1.09$ is all but
 eliminated by a slit (SH2) in front of
 plane I

Note:

Ions with $A/Z \sim 2$ are not separated !

Achromatic magnet separator with Wedge

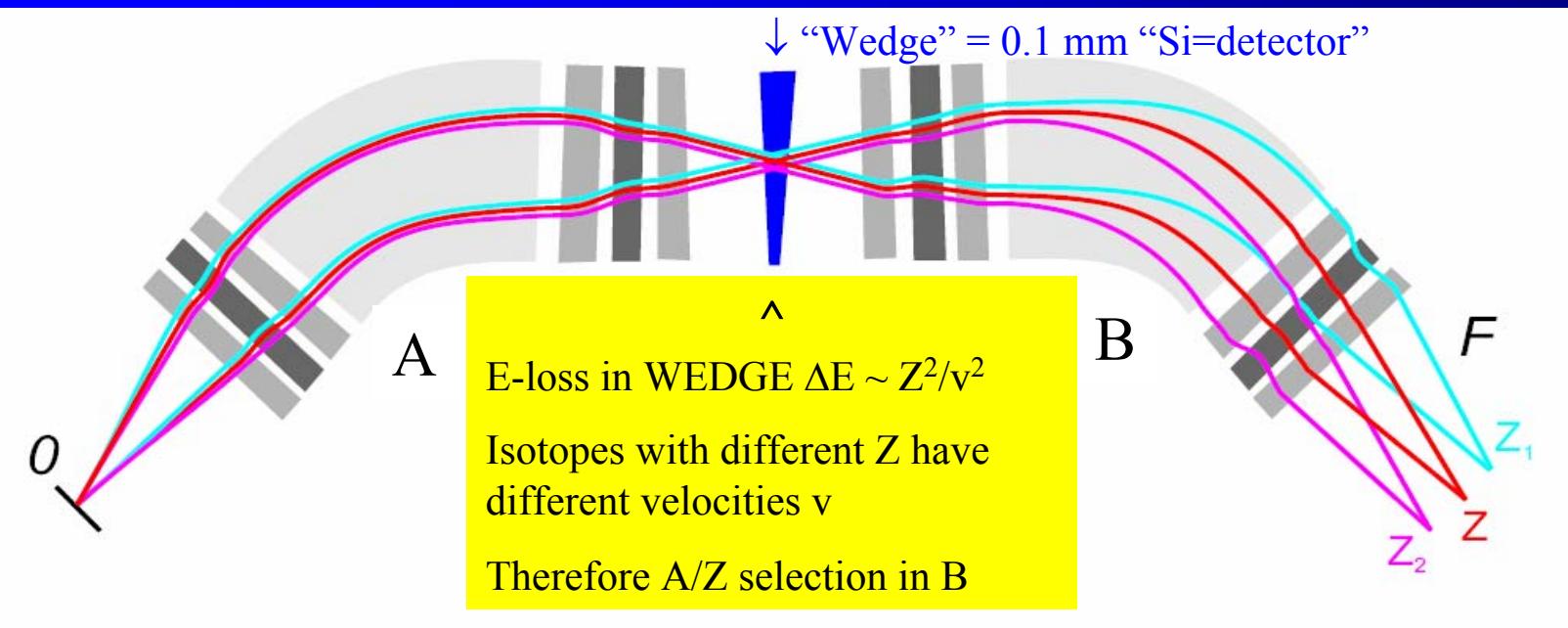
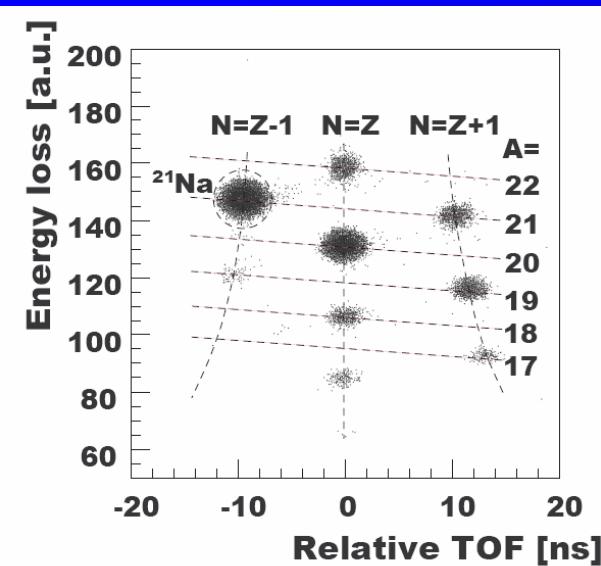


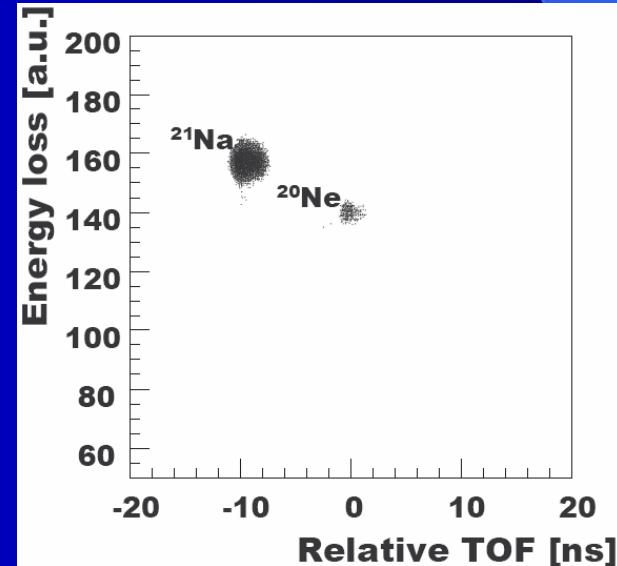
Figure from Experimental Techniques at NSCL, MSU, Th. Baumann, 8/2/2002



Effect of “Wedge” \Rightarrow

Note:

For large $d\mu/p$ the degrader should be Wedge-shaped to restore achromativity effected by degrader with constant thickness

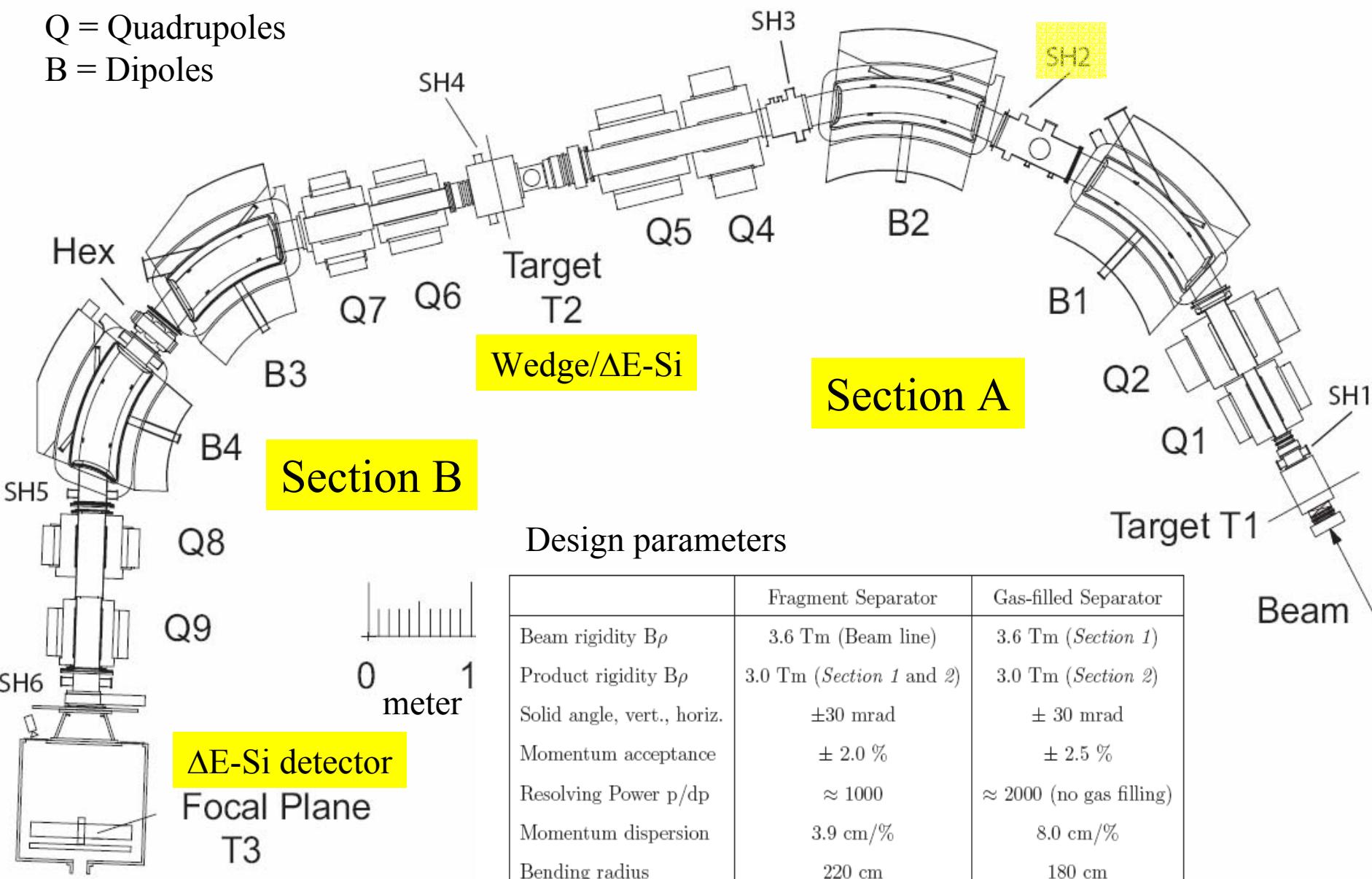


TRI μ P an achromatic secondary beam separator

SH = Slits

Q = Quadrupoles

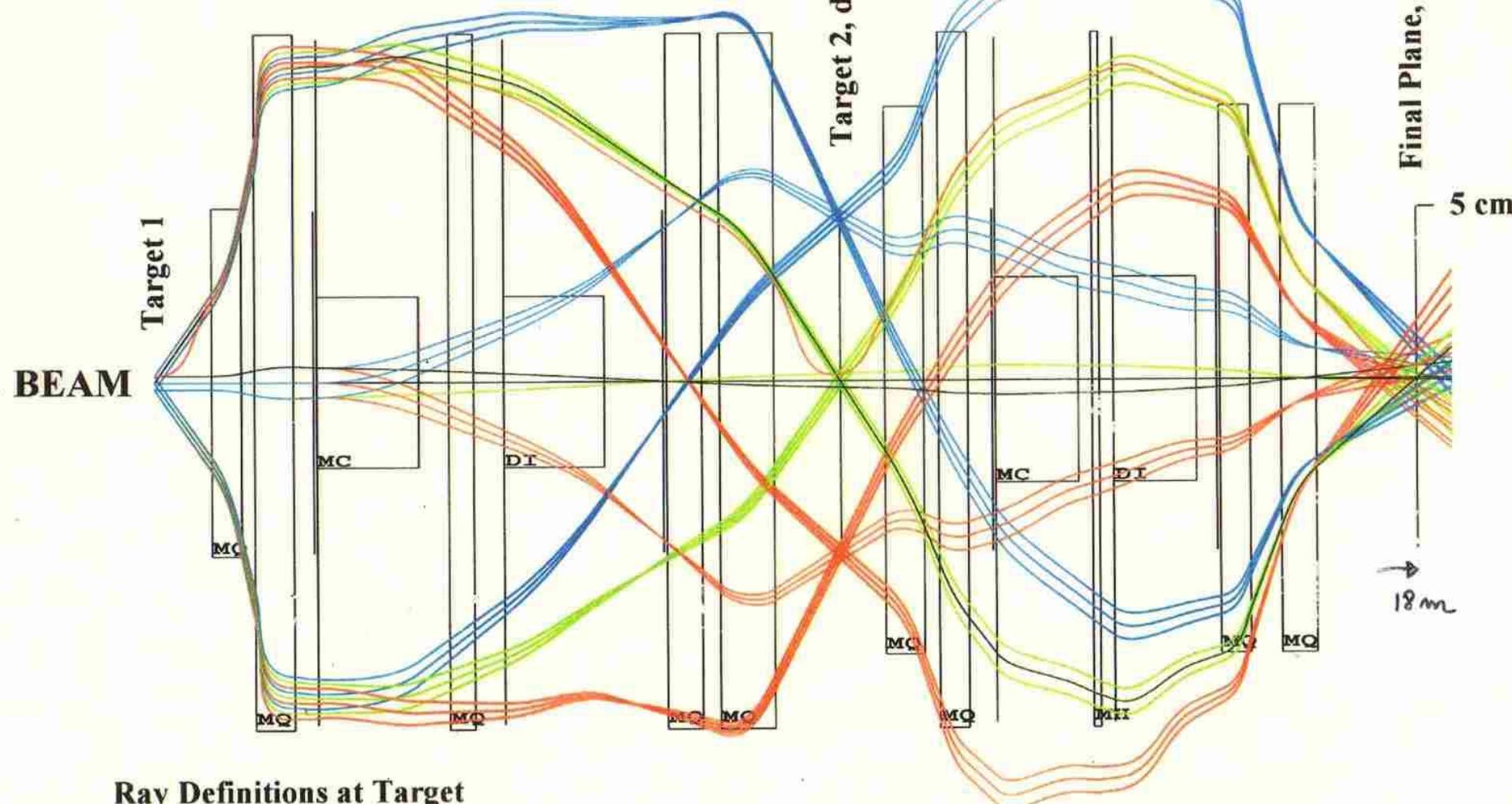
B = Dipoles



TRI μ P Fragment Separator

3rd order COSY Infinity Calculation

Horizontal Plane



Ray Definitions at Target

$$x = +/- 2 \text{ mm}$$

$$\theta = +/- 30 \text{ mrad}$$

$$dp = +/- 2.5 \%$$

TRI μ P ion-optics

Final Plane, achrom.

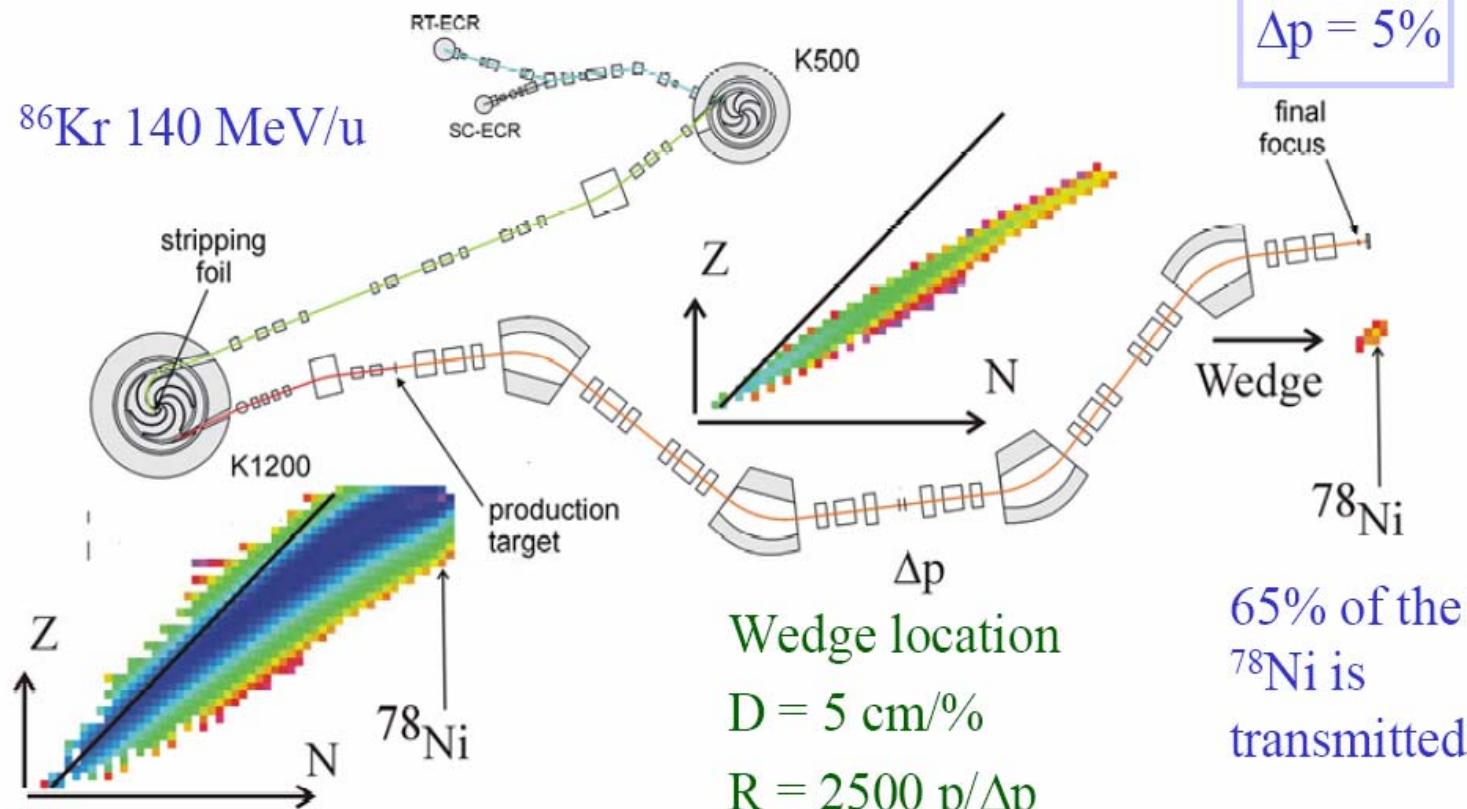
5 cm

18 m

A1900 MSU/NSCL Fragment Separator

Overview of the Fragment Separation Technique

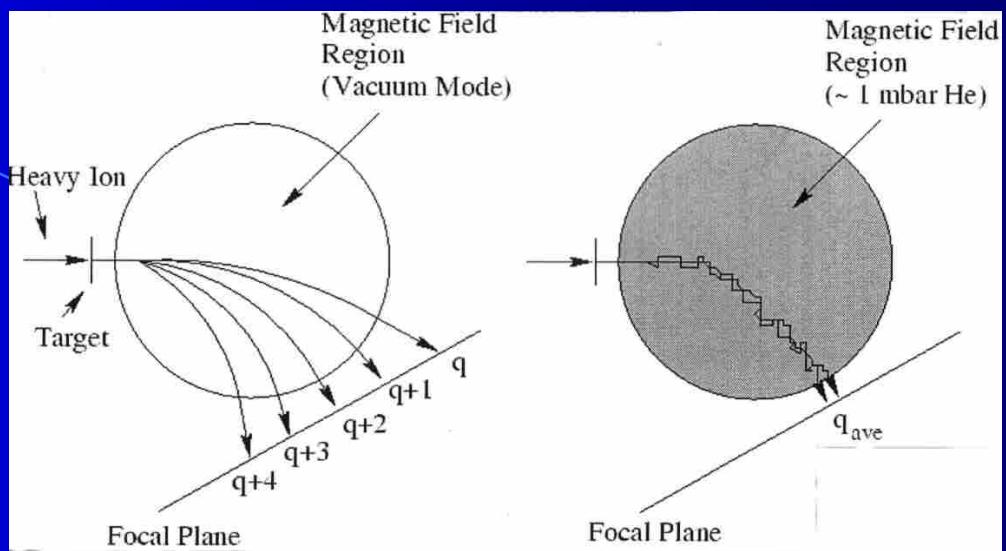
The NSCL Coupled Cyclotron Facility – A1900 Separator



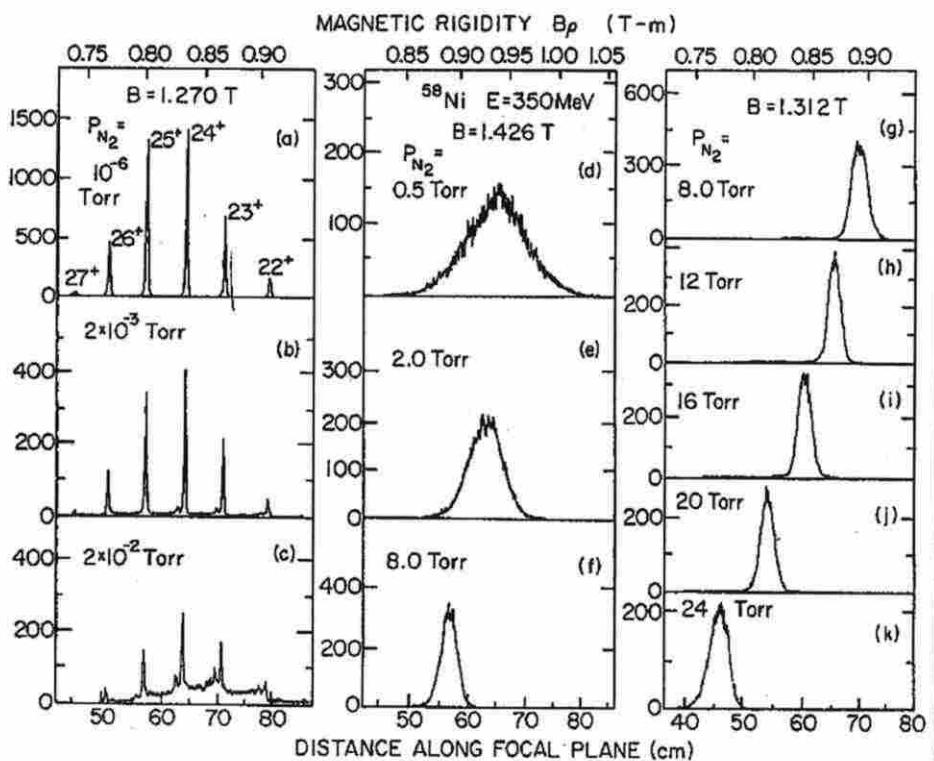
Gas-filled separators Concept

PROBLEM: After target, a distribution of several charge states q exists for low E or large Z , with $B\rho$ range typically larger than acceptance causing transmission losses.

REMEDY: gas-filled separator



M. Paul et al. / Heavy ion separation

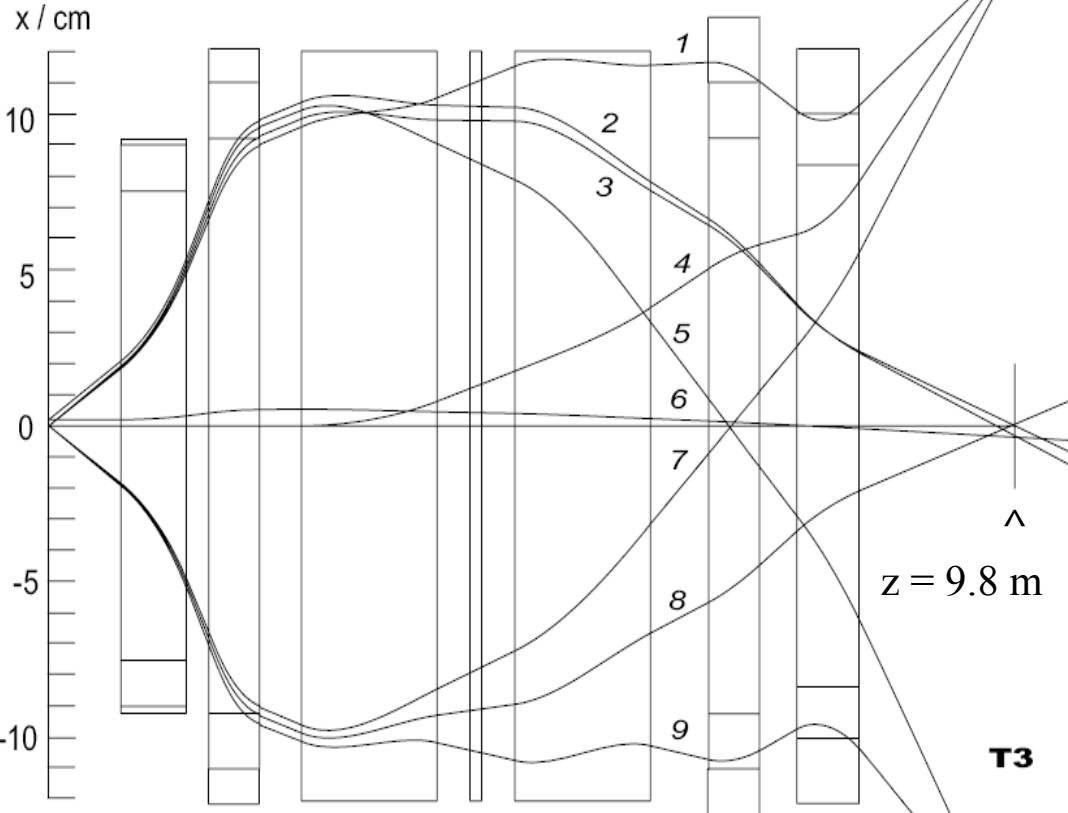


Rays in a magn. dipole field
without and with gas-filling

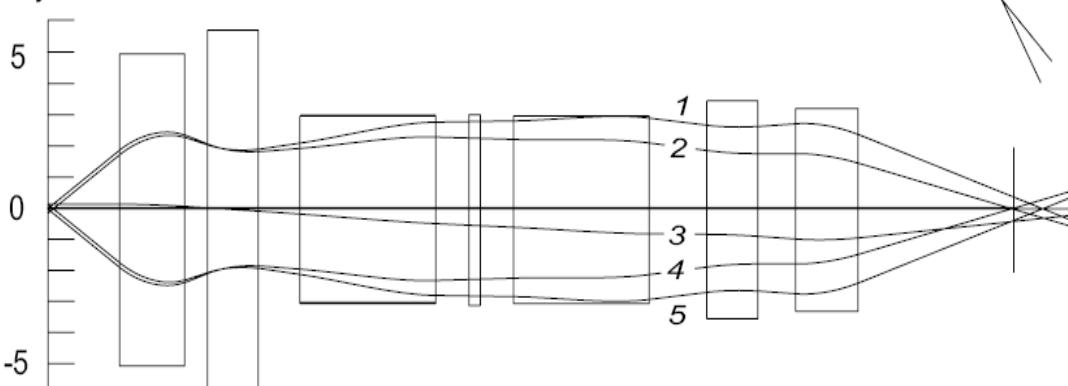
Measured spectra as function of
gas pressure (e.g. He, Ar)

TRI μ P ion-optics Section B

A “long” achromatic separator system is not suitable for a gas-filled separator that should be “short” to reduce statistical E spread and have “large dispersion”



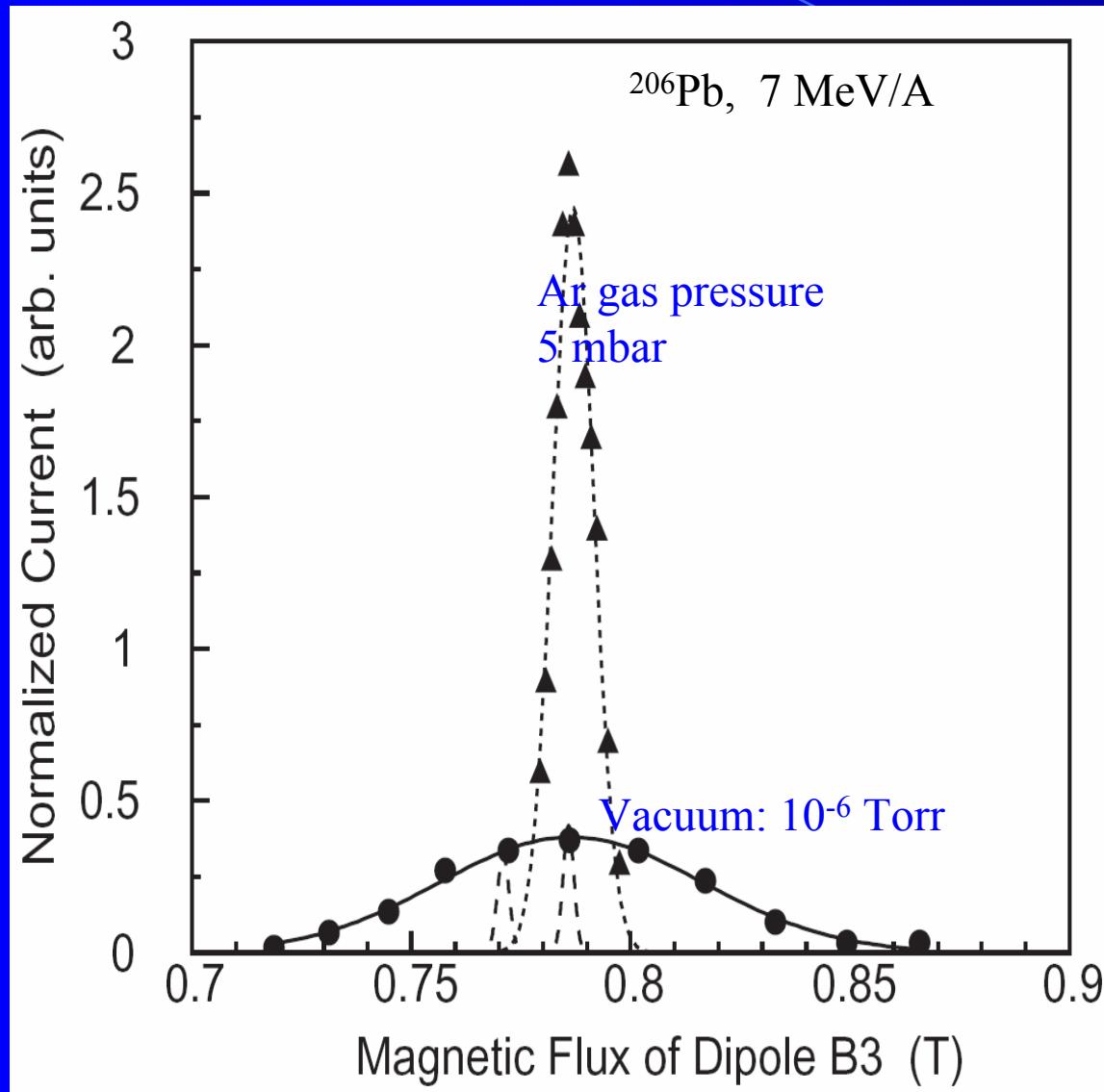
ray	x [mm]	Θ [mrad]	$\Delta E/E [\%]$	y [mm]	Φ [mrad]
1	0	30	4.0	-1.5	30
2	2	30	0	0	30
3	0	30	0	1.5	0
4	0	0	4.0	0	-30
5	0	30	-4.0	1.5	-30
6	2	0	0	0	
7	0	-30	4.0		
8	0	-30	0		
9	0	-30	-4.0		



Therefore:

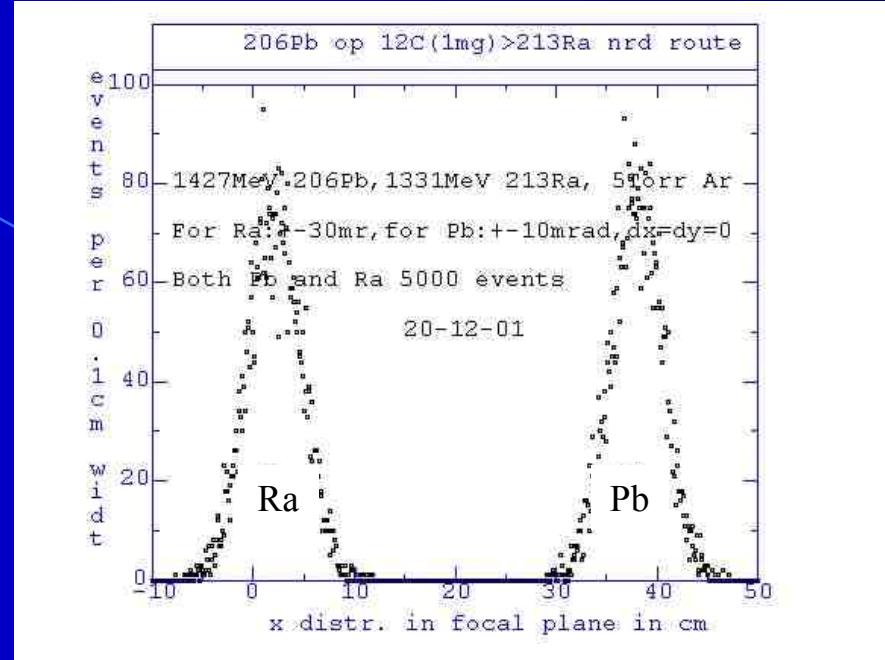
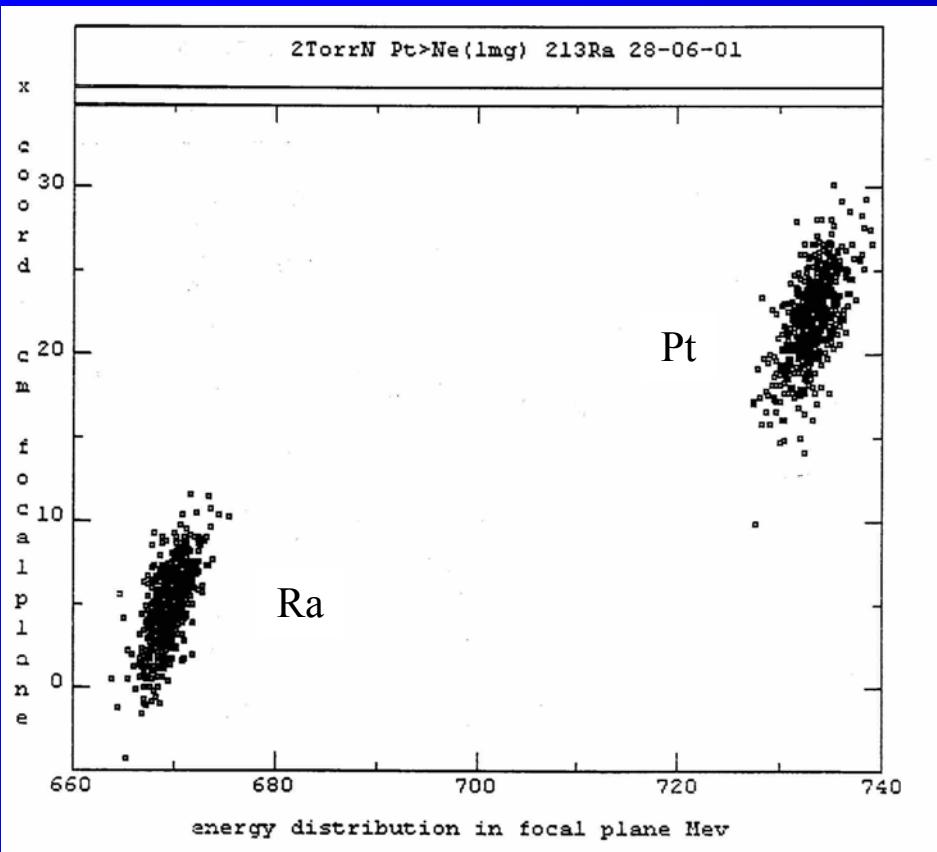
The TRI μ P separator was designed to be able operate with Section A as beam line & Section B as short gas-filled separator with large dispersion

Charge state distribution in TRI μ P separator with gas-filling



RAYTRACE with gas-filling

Modified RAYTRACE code used to calculate the separation of beam to demonstrate particle and beam separation in the TRI μ P separator in Gas-Filled Mode



Recoil Separator St. George

Study of (α, γ) and (p, γ) of astrophysics importance,
for $A < \approx 40$ targets,
emphasis on low energies, i.e. very small cross sections,
max. energy given by KN

An overview of reaction result in the following
DESIGN PARAMETERS

Maximum magnetic rigidity $B\beta$: 0.45 Tm

Minimum magnetic rigidity $B\beta$: 0.10 Tm

Momentum acceptance $d\beta$: +/- 3.7 %

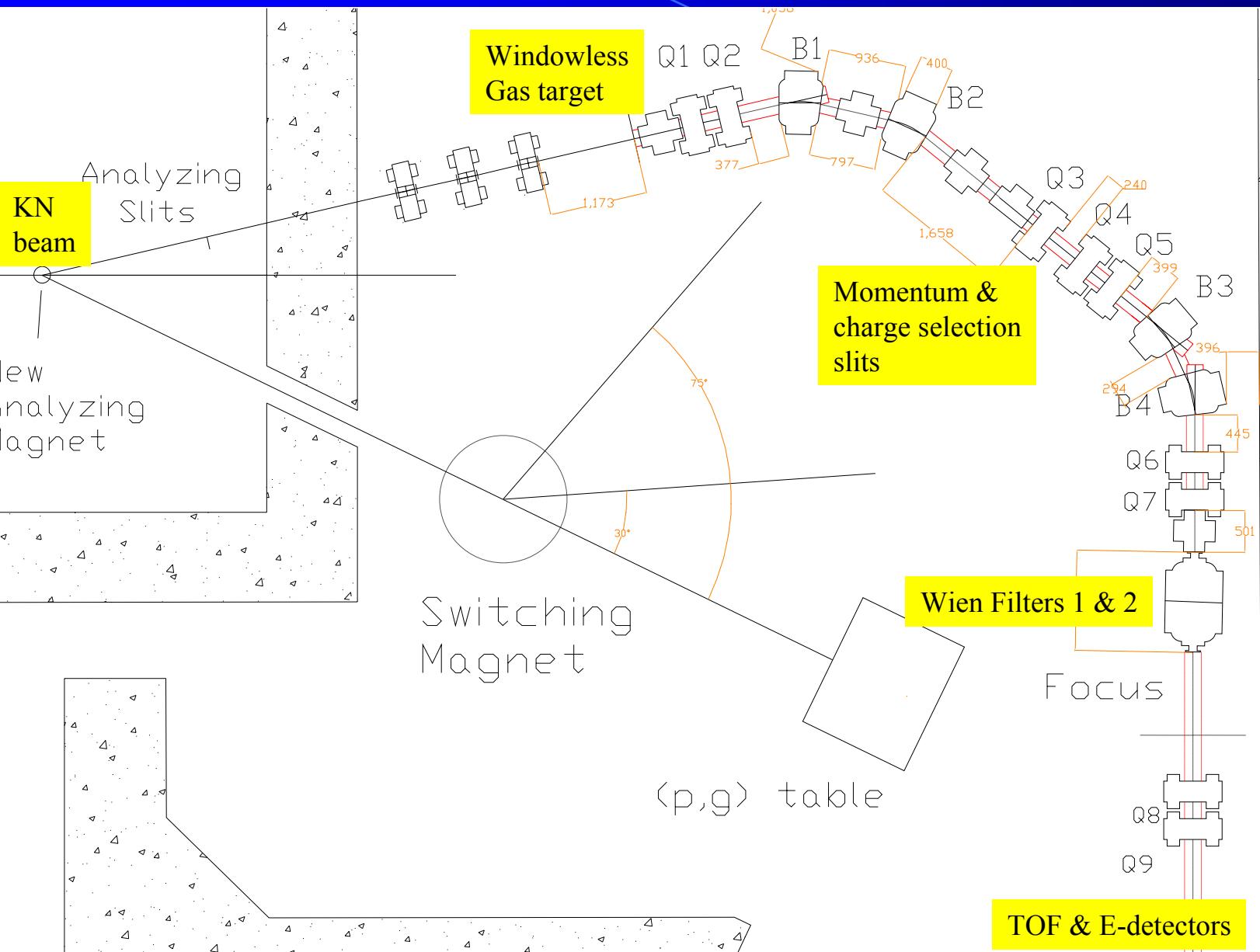
Angle acceptance, horiz & vert.: +/- 40 mrad

Further design considerations:

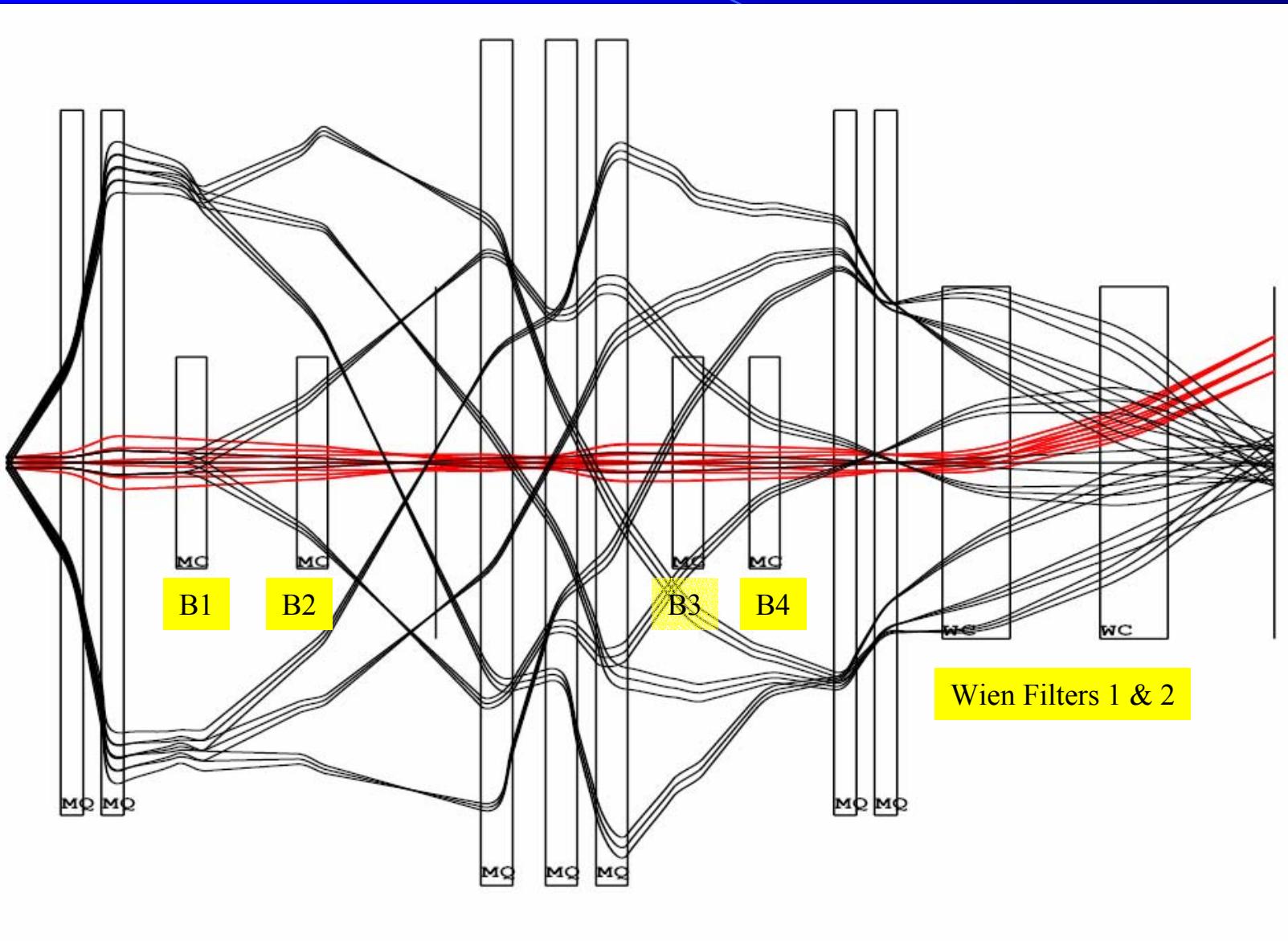
- Two phase construction
- Charge selection by $B\beta$ analysis (typical: 50% Transmission)
- High mass resolution ($\Delta m/m \cong 200$, 1st phase with 2 Wien Filters)
- Higher mass resolution ($\Delta m/m \cong 600$) 2nd phase
- Wien Filters for mass resolution (energy too low for “Wedge” method)

Schematic Floorplan St. George

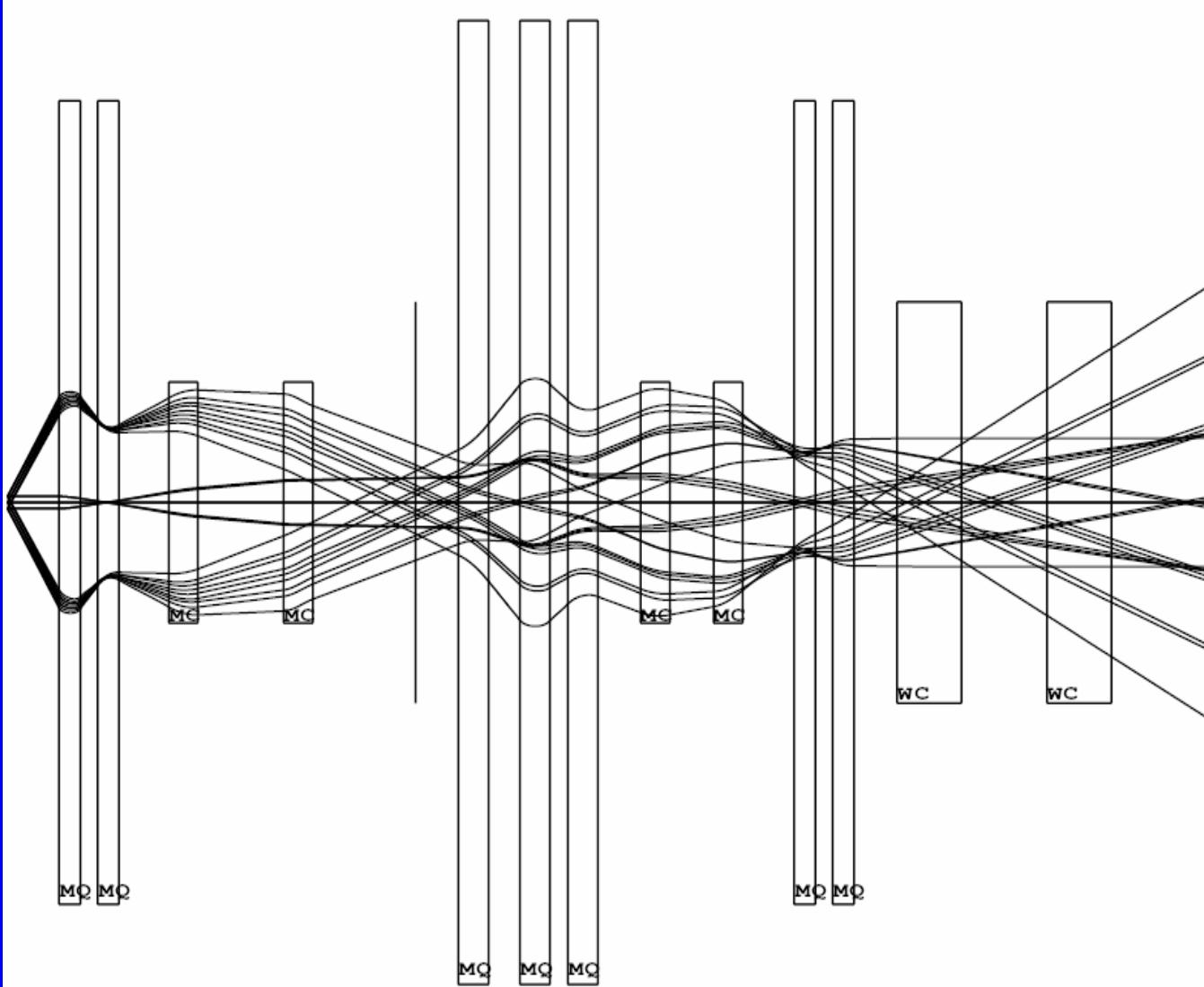
Phase 1



Horizontal ion-optics St. George

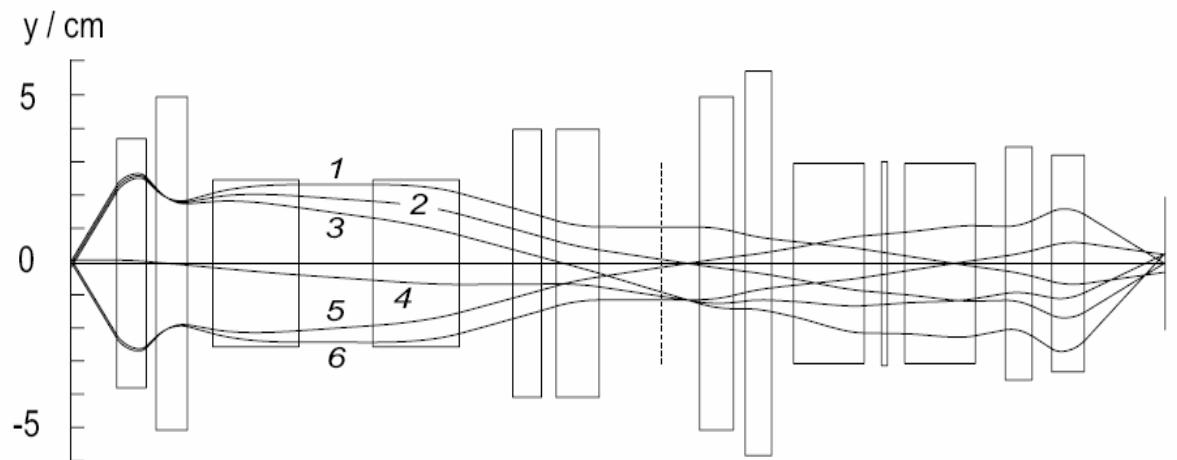
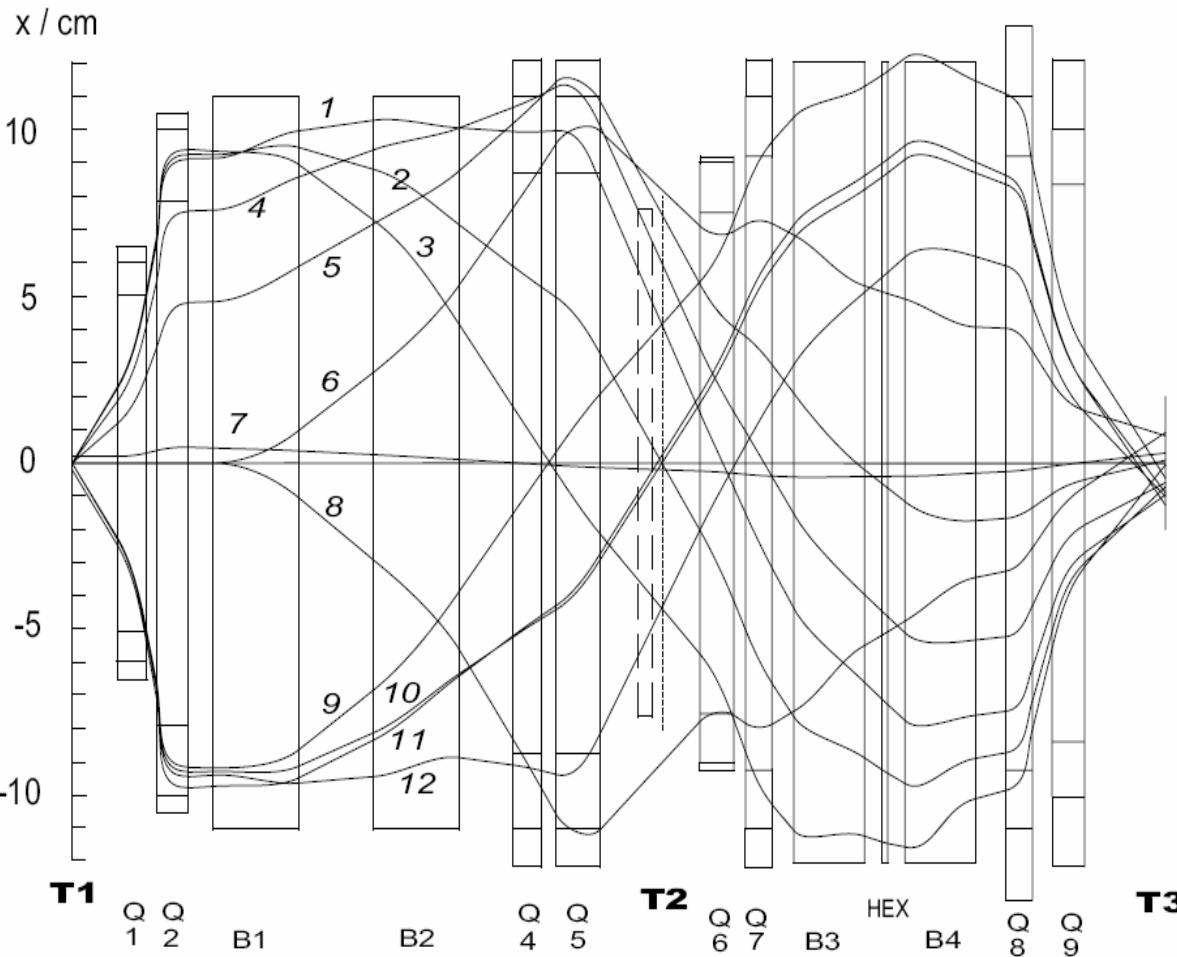


Vertical ion-optics St. George



End Lecture 5

TRI μ P ion-optics 1st & 2nd Section



ray	x [mm]	Θ [mrad]	$\Delta E/E [\%]$
1	0	30	2.2
2	0	30	0
3	0	30	-2.2
4	0	25	3.2
5	0	16	4.0
6	0	0	4.4
7	2	0	0
8	0	0	-4.4
9	0	-30	2.2
10	0	-30	0
11	-2	-30	0
12	0	-30	-2.2

y [mm]	Φ [mrad]
-1	30
0	30
1	30
1	0
0	-30
1	-30